

Great Yarmouth Third River Crossing Application for Development Consent Order

Document 6.2: Environmental Statement

Volume II: Technical Appendix 11D: HAWRAT

Assessment

Planning Act 2008

The Infrastructure Planning (Applications: Prescribed Forms and Procedure) Regulations 2009 (as amended) ("APFP")

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1 HAWRAT Assessment

1.1 Introduction

- 1.1.1 The assessment informs Chapter 11: Road Drainage and the Water Environment of the Environment Statement (ES) in relation to potential impacts of the Great Yarmouth Third River Crossing ("the Scheme"), specifically highway runoff, on water quality.
- 1.1.2 The Scheme will increase impermeable road surface and alter the current traffic flow regime. This has the potential to affect the volume and quality of surface water runoff from the road surface that in turn may affect the quality of the receiving water environment. The purpose of this assessment is to assess the potential impact of the Scheme on the chemical quality of the water environment.
- 1.1.3 The approach that has been adopted follows the approach promoted in Method A and Method D of the Design Manual for Roads and Bridges (DMRB) Volume 11, Part 10, Section 3 (Ref 11D.1):
 - Method A is used to assess pollution impacts from routine runoff to surface waters; and
 - Method D is used to assess pollution impacts from accidental spillage.
- 1.1.4 The methods are implemented using the DMRB HAWRAT assessment tool.
- 1.1.5 Method C is used to assess pollution impacts from routine runoff to groundwater. However, the disposal of road runoff via infiltration is not proposed in the Drainage Strategy (Appendix 12C (document reference 6.2)) due to high groundwater levels in the Principal Application Site and any drainage features will be lined to limit any infiltration of polluted runoff to the underlying groundwater. As such the effects of routine runoff on groundwater are considered negligible, therefore Method C has not been undertaken as part of the HAWRAT assessment.
- 1.1.6 The HAWRAT assessment focusses on permanent risks during the operational phase of the Scheme and does not consider risks during the construction phase as the methodology is not appropriate for assessing impacts associated with construction traffic. Potential impacts to chemical water quality during construction are qualitatively assessed within Section 11.8 of Chapter 11: Road Drainage and the Water Environment.



1.2 Assessment Parameters

- 1.2.1 The Scheme involves the construction, operation and maintenance of a new crossing of the River Yare in Great Yarmouth. The Scheme consists of a new dual carriageway road, including a road bridge across the river, linking the A47 at Harfrey's Roundabout on the western side of the river to the A1243 South Denes Road on the eastern side.
- 1.2.2 The Scheme aims to relieve traffic that at present must travel through the town centre and will increase traffic flows in the immediate vicinity of the Principal Application Site. The forecast with-Scheme 24-hour two-way Annual Average Daily Traffic (AADT) flow for the 2038 scenario is estimated as 18,195 for the existing William Adams Way adjacent to Harfrey's Roundabout, compared with 15,608 under the baseline condition. The forecast AADT traffic flows for the new bridge crossing and highway (including the new roundabout) are estimated as 23,041. Both the baseline and forecast with-Scheme traffic flows are in the lowest range assessed using the HAWRAT tool, ≥ 10,000 to < 50,000. Approximately 4% of this will comprise Heavy Goods Vehicles (HGVs).
- 1.2.3 New highway drainage is proposed for the Scheme and the key principles of the Drainage Strategy (Appendix 12C (document reference 6.2)) are stated as follows:

The western side of the Scheme - the section of the Scheme due west of the bridge mid-point (Total area = 3.3ha)

- Runoff from the western side of the Scheme will be attenuated and discharged either via gravity into the existing Internal Drainage Board (IDB) ordinary watercourse network adjacent to the Scheme or via a pumped system into the River Yare. This assessment investigates the potential effects of both discharge options.
- Runoff to be attenuated to as close as practical to greenfield runoff rates for the 1 in 100-year event, including climate change. Where this is not achievable, the post development runoff rates and volumes should not exceed existing scenario values. The required attenuation storage will, as a minimum, consist of an underground storage tank and a pond/wetland feature.
- Runoff will be treated before discharge. Pollution control measures will include proprietary treatment devices (vortex separator) and natural treatment in the form of wet pond/wetland feature. Penstocks are also proposed as control of spillages.



The eastern side of the Scheme - the section of the Scheme due east of the bridge mid-point (Total area=0.9ha)

- Runoff from the eastern side of the Scheme will be discharged into existing Anglian Water combined sewer.
- Runoff to be attenuated, via oversized pipes and/or underground storage tanks, to achieve the restricted discharge rate of 10l/s as agreed with Anglian Water.
- Runoff to be treated, via proprietary devices, before discharge into the Anglian Water combined sewer.
- 1.2.4 The proposed drainage areas for the western and eastern side of the Scheme were estimated based on the General Arrangement Plans (document reference 2.2), which include a combination of permeable and impermeable area that contribute to the respective outfalls. In order to account for the limits of deviation that will allow for minor changes to the highway design and subsequently the drainage areas for the Scheme, the HAWRAT assessment has investigated the potential effects of increasing the impermeable surface area by 15%. Given the limited space within the Principal Application Site, it is not expected that the drainage areas would deviate by more than 15%.

1.3 Assessment Approach: Method A

Scope of the Assessment

- 1.3.1 Method A assesses the risks of water pollution within the receiving watercourse associated with the proposed routine discharges from the Scheme. The assessment has only been completed for the western side of the Scheme, which is currently known to discharge into the IDB watercourse network adjacent to the Scheme. The drainage catchment for this side of the Scheme has an impermeable area of 2.5ha based on the General Arrangement Plans (document reference 2.2). The assessment has also considered the potential impacts of increasing the impermeable area by 15% (i.e. up to 2.88ha) to allow for the limits of deviation provided for in the DCO.
- 1.3.2 Highway runoff from the eastern part of the Scheme will undergo two stages of treatment; first via proprietary devices installed as part of the Scheme Drainage Strategy (Appendix 12C (document reference 6.2)), prior to discharge into Anglian Water combined sewer, and second where discharged runoff will be treated alongside existing flows as part of Anglian Water's treatment processes. Given discharges from the eastern side of the Scheme will be incorporated into Anglian Water's treatment system, and Anglian Water has confirmed this will not affect the performance of their



sewage treatment works, the effects have not been considered further in this assessment.

1.3.3 Two separate HAWRAT assessments have been completed:

- Scenario 1: Discharge to the existing IDB watercourse network adjacent to the Scheme. This IDB network, which forms part of the surface water drainage for the urban areas of Great Yarmouth, is connected to the wider network of dykes and drains within the Waveney, Lower Yare & Lothingland IDB district. Water level within the IDB district is managed by pumping, which removes excessive runoff from the marshes, urban area and the upland catchment to the River Yare.
- Scenario 2: Discharge to the River Yare. The River Yare is a transitional tidal waterbody through Great Yarmouth. The HAWRAT tool, used in this assessment, was designed to assess the impacts to freshwater bodies and is therefore not directly applicable to the assessment of impacts to transitional waters. Furthermore, given the size of the River Yare catchment at the Principal Application Site (estimated to be around 3,130km²), its current use for commercial and recreational navigation, and the regular dredging activities to remove accumulated sediment, it is considered highly unlikely that the Scheme would pose a notable risk to water quality. However, in order to quantify and therefore better understand the scale of potential impact, the HAWRAT assessment process has been applied to a freshwater scenario to enable consideration of likely pollutant concentrations and dilution requirements.

1.3.4 Two types of assessment are undertaken within the HAWRAT tool:

- Short-term impacts on aquatic ecology related to the intermittent nature of road runoff. For an individual outfall to pass the HAWRAT assessment it must pass both the soluble pollutant and sediment pollutant impacts.
- Long-term impacts based on annual average concentration of certain hazardous pollutants, as defined under the Water Framework Directive (WFD). The long-term risks over the period of one year are assessed through comparison of the annual average concentration of pollutants discharged with the published Environmental Quality Standards (EQS) for those pollutants.
- 1.3.5 HAWRAT is a tiered consequential system which involves up to three assessment stages, outlined as 'steps' within the assessment spreadsheet. These are detailed as follows:
 - Step 1 uses statistical models to determine pollutant concentrations in raw road runoff prior to any treatment or dilution in the receiving watercourse;



- Step 2 assess pollutant concentrations after dilution and dispersion in the receiving watercourse, but without active mitigation; and
- Step 3 considers the pollutant concentrations with active mitigation. Pollution control measures proposed as part of the Drainage Strategy (Appendix 12C (document reference 6.2)) will include a vortex separator to treat runoff that discharges into the underground storage tank and natural treatment in the form of wet pond/wetland feature. However, the proportion of the Scheme (western side) contributing to the underground storage via the vortex separator and the proportion contributing to the pond/wetland feature are currently unknown. Hence, it is assumed that the entire western side of the Scheme will contribute to the underground storage via the vortex separator to provide the worst-case scenario. A vortex separator is effective in the removal of fine sediment, sediment-bound pollutants and hydrocarbons. However, its ability to remove soluble metals is considered limited.

Assessment Parameters

1.3.6 Information used to complete the HAWRAT assessments for both discharge scenarios are summarised in Table 1.1

Table 1.1: Summary of Input Data for HAWRAT Assessments

Input Data	Discharge	Locations
Iliput Data	IDB Watercourse	River Yare
Impermeable area	2.5 (and 2.88 to allow for	2.5 (and 2.88 to allow for
drained to outfall (ha)	limits of deviation)	limits of deviation)
Permeable area drained to outfall (ha)	0.8	0.8
Standard Average Annual Rainfall (SAAR)	550mm based on rain gauges from nearby stations	550mm based on rain gauges from nearby stations
Base Flow Index (BFI) ¹	0.73	0.64
Water hardness	A low value of < 50mg CaCO ₃ /L was selected as a reasonable worst case as this information is uncertain	A low value of < 50mg CaCO ₃ /L was selected as a reasonable worst case as this information is uncertain
Estimated river width (m)	2	100

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¹ Derived using the LowFlows 2 software based on characteristics of the catchment.



Input Data	Discharge	Locations
iliput Data	IDB Watercourse	River Yare
Is the discharge in or within 1km upstream of a protected site for conservation?	No international / national designated conservation sites have been identified within 1km downstream from the point of discharge (the Breydon Water SSSI is located approximately 2km from the point of discharge)	Yes, the River Yare is included in the Outer Thames Estuary Special Protection Area (SPA)
Is there a downstream structure, lake, pond or canal that reduces the velocity within 100m of the point of discharge?	The IDB watercourse network is culverted in many places and a culvert structure is found within 100m of the point of discharge.	No - although on flood tides reverse flow occurs in the Yare at the point of discharge, the assessment has been undertaken assuming minimal flow (i.e. periods of slack tide when fluvial flow dominates).

Determining the Annual 95% River Flow

- 1.3.7 The HAWRAT tool requires an estimation of the 95 percentile (%) river flow to represent likely low flow conditions (and therefore potential for greatest impact). Consultation with the Environment Agency and the IDB has confirmed that they do not carry out or hold any flow measurements for the IDB watercourse network adjacent to the Scheme. It is expected that flows would be intermittent due to tidal influences and the largely urbanised nature of the catchment. Hence it is difficult to produce representative annual 95 percentile (%) river flows (Q95s) that feed into the assessment to determine the pollutant concentrations after dilution and dispersion in the receiving watercourse. Furthermore, given the potential ephemeral nature of the watercourse, the dilution capacity is likely to be limited with Q95s close to zero at times, in particular for the drier summer months.
- 1.3.8 According to the guidance provided in the DMRB (Ref 11D.1), if the Q95 value is less than 0.001m³/s, a figure of 0.001m³/s should be used in the assessment. Due to the uncertainties associated with the flow rates and duration of the receiving watercourse, the assessment has been carried out based on a Q95 value of 0.001m³/s, i.e. the lowest value that should be used



in the assessment, to reflect the limited dilution capacity of the watercourse and therefore the worst case.

1.3.9 Estimating an appropriate Q95 for the River Yare is equally problematic due to the transitional nature of the waterbody as it is influenced by both fluvial flows from the upper catchment and tidal inflows from the North Sea. The fluvial Q95 value has been used for this assessment, with no consideration of tidal inflows. This is considered a reasonable worst-case scenario as it represents the lowest flow rate in the River Yare, during periods of slack tide, when the dilution capacity is at its lowest. The river has a catchment area of around 3,130km² at the Principal Application Site and the Q95 flow was estimated to be approximately 4.5m³/s.

Summary of Assessment

Scenario 1: Discharge to existing IDB watercourse network

1.3.10 The Scheme failed Step 1 of the HAWRAT assessment, which is the assessment of pollutant concentrations in raw road runoff prior to any treatment or dilution in the receiving watercourse. The findings of Step 2 and Step 3 of the HAWRAT assessment, which assess pollutant concentrations after dilution and dispersion in the receiving watercourse without and with active mitigation, respectively, are summarised in Table 1.2 (details provided in Annex A), with a review of this assessment provided below.



Table 1.2: Summary of HAWRAT Assessment of Pollution Risks to IDB Watercourse

		Short Te	rm Pollutant Im	pacts	Long Term Pollutant Impacts			
Assessment stage	Impermeable area (ha)	Acute impact assess ment of Copper	Acute impact assessment of Zinc	Sediment (chronic impact)	Annual average concentration of Copper (µg/l) due to road runoff	Annual average concentration of Zinc (µg/l) due to road runoff		
Step 2 (no mitigation)	2.5	FAIL	FAIL	FAIL	0.79	1.79		
Step 3 (with mitigation)	2.5	FAIL	FAIL	PASS* (but alert due to presence of downstream structure)	0.79	1.79		
Step 2 (no mitigation)	2.88	FAIL	FAIL	FAIL	0.86	1.95		
Step 3 (with mitigation)	2.88	FAIL	FAIL	PASS* (but alert due to presence of downstream structure)	0.86	1.95		
* The vortex separate	or is assu	med to have	80% removal capa	bility for fine sediment. ²				

² Percentage removal is based on industry design standard for a hydrodynamic vortex separator - information provided by Hydro International for their product, Downstream Defender, which is an advanced hydrodynamic vortex separator (Ref 11D.2).



- 1.3.11 The HAWRAT tool indicates the acute concentration of pollutants generated by the Scheme would exceed the acceptable threshold values for both Copper and Zinc set by the DMRB methodology (Ref 11D.1), thus failing the assessment of short-term pollutant impacts. Due to the presence of culvert structures along the IDB watercourse, which could potentially lower the flow velocity, the HAWRAT tool also indicates there would be extensive settlement of sediments, causing the watercourse to fail the assessment of sediment-bound pollutants. Given the ephemeral nature of the IDB watercourse, there is insufficient dilution to pass the HAWRAT assessment without active mitigation.
- 1.3.12 With the incorporation of the vortex separator as pollution control, the Scheme would pass the assessment of sediment-bound pollutants, but there remains a risk of impact due to the presence of a culvert structure downstream from the point of discharge, which could potentially reduce flow velocity and encourage the deposition of sediment. However, the volume of sediment entering the receiving watercourse following mitigation would be small, hence the effect of the downstream structure is considered to be insignificant.
- 1.3.13 The Scheme still fails the assessment of short-term pollutant impacts due to the limited capability of the vortex separator to remove soluble metals. However, it is important to note that the current assessment assumed the worst case whereby the entire western part of the Scheme was assessed to contribute to the underground storage via the vortex separator. It is understood that a proportion of the Scheme would discharge into a wet pond, which has the potential to remove up to 50 - 80% of soluble heavy metals, according to Table 3.7 of CIRIA C609, Sustainable drainage systems - Hydraulic, structural and water quality advice (Ref 11D.3). Furthermore, the CCTV survey conducted as part of the Drainage Strategy (Appendix 12C (document reference 6.2)) and consultation with the IDB has confirmed that the majority of the existing highway in the vicinity of the Scheme drains into the same IDB watercourse with no known treatment measures incorporated. Given the risk of pollution already exists in this waterbody due to existing highway discharges, runoff from the Scheme is not expected to cause significant deterioration in water quality in the IDB watercourse, even if runoff is discharged untreated.
- 1.3.14 As shown in Table 11D.2, the outcomes and subsequently the conclusion of the assessment of short-term pollutants in the IDB watercourse would remain unchanged with the increase in impermeable road area to account for deviation in highway design for the western side of the Scheme.
- 1.3.15 HAWRAT also provides an assessment of long-term pollution impacts to the receiving water environment, which considers the annual average pollutant concentrations associated with the Scheme against the EQS that inform the WFD. The threshold values in the DMRB (Ref 11D.1) are 1 µg/l in the water



hardness band of < 50mg/l CaCO $_3$ for Copper and 7.8 µg/l in all water hardness bands for Zinc. The results of the HAWRAT assessment indicate annual average concentrations of Copper and Zinc are below these threshold values. With the increase in impermeable area, the concentrations would increase but only marginally and the values are still below the threshold. Therefore, in themselves, discharges from the Scheme would not result in the EQS values being exceeded at the point of discharge. The EQS values may be exceeded when taking into account existing discharges to the local IDB drains, however the estimated topographical catchment to the point of discharge is approximately 2 km², comprising large areas of urban development and highway. The drained area from the Scheme (~ 3.3 ha based on current highway design and ~3.7 ha that allows for deviation) represents less than 2% of this catchment, therefore discharges from the Scheme will not significantly affect the water quality in these drains.

1.3.16 Contaminants released into the IDB watercourse network adjacent to the Scheme could be transported downstream to impact on the water quality of the wider network of dykes and drains within the IDB district, in particular the more sensitive marshland south of Breydon Water. However, a comparison of the catchment areas at the point of discharge (approximately 2km²) and at the marshland (approximately 12km²), suggests the contaminants would have been sufficiently diluted and dispersed before reaching the main dyke system within the marshes (Plate 1.1). It is therefore highly unlikely that highway discharges from the Scheme would have any significant effect on the water quality of the wider IDB catchment.



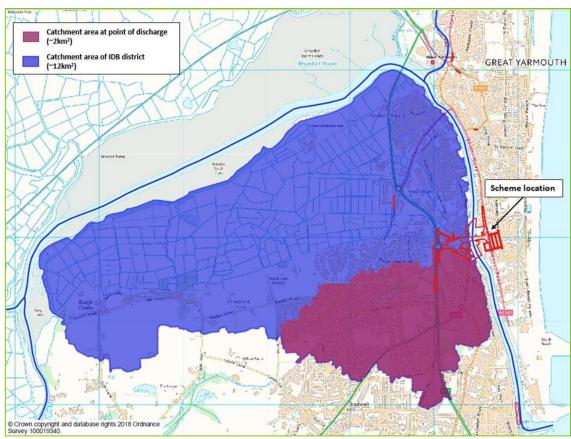


Plate 1.1: A Comparison of the Wider IDB Catchment and the Catchment at the Point of Discharge

Scenario 2: Discharge to the River Yare

1.3.17 With the option of discharging into the River Yare, the Scheme would pass Step 2 of the HAWRAT assessment, which takes into account dilution and dispersion in the river, without active mitigation being necessary. Table 1.3 summarises the findings of the Step 2 assessment (details provided in Annex A), with a review of this assessment provided below.



Table 1.3: Summary of HAWRAT Assessment of Pollution Risks to the River Yare

မ	(ha)	Short Ter	m Pollutant Imp	Long Term Pollutant Impacts		
Assessment stage	Impermeable area (Acute impact assessm ent of Copper	Acute impact assessment of Zinc	Sediment (chronic impact)	Annual average concentration of Copper (µg/l) due to road runoff	Annual average concentration of Zinc (µg/l) due to road runoff
Step 2 (no mitigation)	2.5	PASS	PASS	PASS (but alert as runoff is discharged into a protected area)	0.00	0.00
Step 2 (no 2.88 mitigation)		PASS	PASS	PASS (but alert as runoff is discharged into a protected area)	0.00	0.00



- 1.3.18 The HAWRAT tool indicates the acute concentration of pollutants generated by the Scheme would be below the acceptable threshold values set by the DMRB methodology (Ref 11D.1), with consideration of the dilution potential within the River Yare. It is anticipated that the dilution capacity of the river would be significantly greater than that assessed in the HAWRAT, due to tidal flows which were not considered in the assessment. Hence, the Scheme is not expected to pose a short term pollution risk to this waterbody. The results for the assessment of sediment deposition indicate there would be limited settlement of sediment and associated sediment-bound pollutants in the River Yare. However, the assessment still alerted a potential risk of impact because the River Yare is included in the Outer Thames Estuary SPA. Given the river is already regularly dredged for navigation, the potential increase in sediment and sediment-bound pollutants associated with highway discharges from the Scheme is not considered to pose a notable impact.
- 1.3.19 With respect to long-term pollution impacts, the results of the HAWRAT assessment indicate annual average concentrations of Copper and Zinc associated with the Scheme would be zero. This is to be expected given the significant dilution capacity of the River Yare. Highway runoff discharges from the Scheme represent a very small proportion of the flow in the Yare and will therefore not have any notable effect on existing pollutant concentrations.
- 1.3.20 It can be seen from Table 11D.3 that the increase in impermeable road area within the limits of deviation has not altered the results of the HAWRAT assessment for the River Yare.
- 1.3.21 Consultation has been carried out with the Environment Agency to request relevant water quality sampling data for the River Yare waterbody. The data showed that both the maximum and annual mean concentrations of the sampled elements, including Arsenic, Ammonia, Mercury, heavy metals such as Cadmium, Lead, Copper, Zinc, and Nonylphenol, are all below the transitional waters EQS used to inform the WFD. This suggests the waterbody is not at pressure relating to these elements, which are contaminants that could be found in road runoff. The HAWRAT assessment shows the Scheme discharges will not lead to a change in existing pollutant concentrations and therefore discharges from the Scheme will not affect the water quality in the River Yare.
- 1.3.22 Step 3 of the HAWRAT assessment was not completed for this scenario as the Scheme passes the HAWRAT assessment at Step 2.



1.4 Assessment Approach: Method D

Scope of the Assessment

- 1.4.1 Method D of the DMRB assesses the risk of pollution from spillages occurring during operation of the Scheme i.e. if an accident were to occur. The assessment considers likely spillage rates based on the nature of the road (i.e. presence of slip roads, roundabouts, junctions, etc. that can increase risk) and the percentage of the AADT that comprises HGVs.
- 1.4.2 The assessment is designed to consider spillage risks to motorways and A-roads and, as such, is not directly applicable to this Scheme given the slower speeds of vehicles using these roads. The assessment will, however, give an indication of potential risks should an accident occur. Similar to the Method A assessment, this assessment has only been completed for the western side of the Scheme. The length of road considered in this assessment measures approximately 645m.

Assessment Parameters

- 1.4.3 The following information has been used to complete the HAWRAT Method D assessment:
 - Outfall will drain to a surface watercourse;
 - The road type was selected as an A-road in an urban area;
 - Response time taken as <20 minutes as the site is urban;
 - Two-way AADT of 23,041 vehicles for the new bridge crossing and highway;
 - 4% HGV traffic.
- 1.4.4 The DMRB (Ref 11D.1) provides spillage rates for different types of junctions and for lengths of road within 100m of these junctions.

Summary of Assessment

1.4.5 A summary of this information is provided in Table 1.4, noting that only new junctions have been considered and that the assessment (details provided in Annex B) has been completed without and with the consideration of mitigation.



Table 1.4: Summary of HAWRAT Assessment of Pollution Impacts from Spillages

<u>-</u>			<u> </u>	, ,			
Assessment type	Type of junction	Length of carriageway within 100m of junction	Spillage rates (Table D1.1 (Ref 11D.1),)	Annual probability of a serious pollution incident			
No mitigation	New five- arm roundabout	420	5.35	0.00034 (0.034%)			
	Carriageway not within 100m of junction	225	0.31	0.00001 (0.001%)			
With mitigation (spillage control penstocks with a	New five- arm roundabout	420	5.35	0.00014 (0.014%)			
pollution reduction factor of 0.4 (60%))	Carriageway not within 100m of junction	225	0.31	0.00000 (0.0%)			

- 1.4.6 The DMRB (Ref 11D.1) recommends that an annual probability of a serious pollution incident occurring of less than 1% would be acceptable. The results of the HAWRAT assessment without the consideration of mitigation indicate a total annual probability of 0.035%, which is well below this threshold.
- 1.4.7 Although the estimated spillage risk is below the DMRB threshold, it is considered good practice to incorporate mitigation measures of spillage containment. The use of penstocks has been proposed as part of the Drainage Strategy (Appendix 12C (document reference 6.2)) to control spillage. According to Table 8.1 of DMRB Volume 11, Part 10, Section 3 (Ref 11D.1), this has the potential to reduce the risk by 60%, which subsequently reduces the annual probability of a serious pollution incident to 0.014%.



2 References

Ref 11D.1: Design Manual for Roads and Bridges Volume 11, Section 3, Part 10 (HD 45/09) Road Drainage and the Water Environment, former Highways Agency, November 2009.

Ref 11D.2: Hydro International (2016, online). Downstream Defender Design Data Sheet.

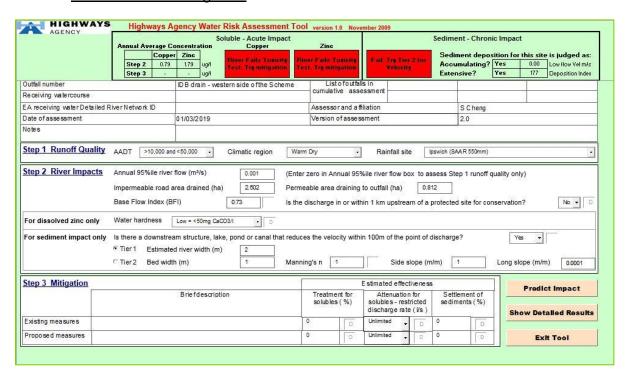
Ref 11D.3: CIRIA (2004). CIRIA C609, Sustainable Drainage Systems – Hydraulic, structural and water quality advice.



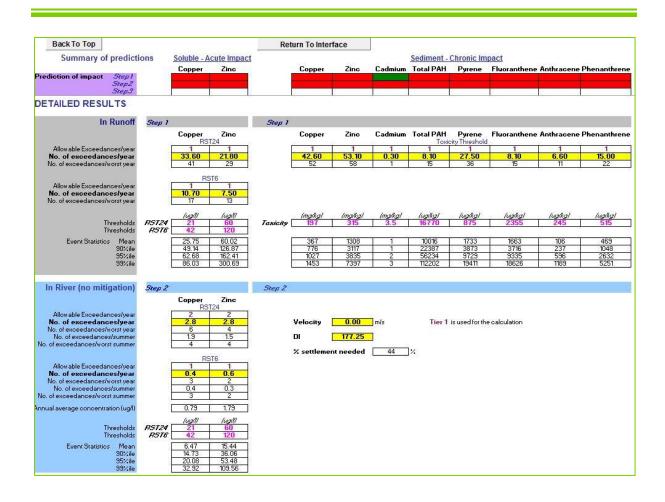
Annex A: Details of the Method A Assessment

Scenario 1: Discharge to existing IDB watercourse (2.5ha impermeable area)

Without Active Mitigation

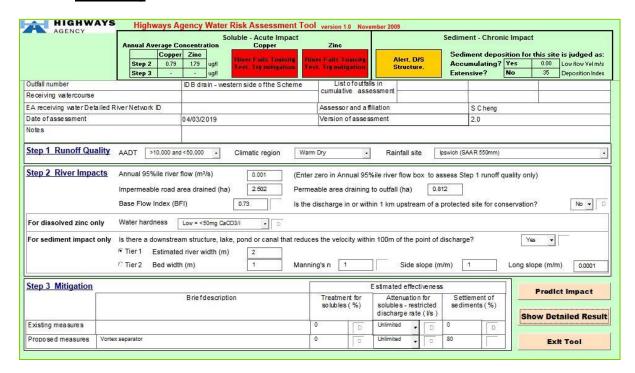


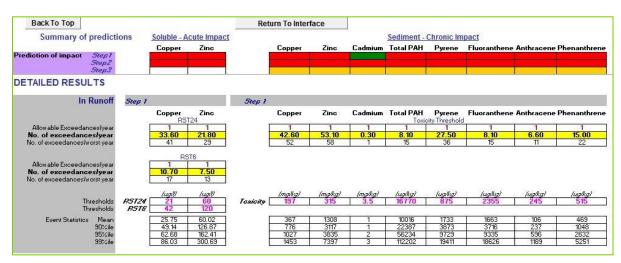




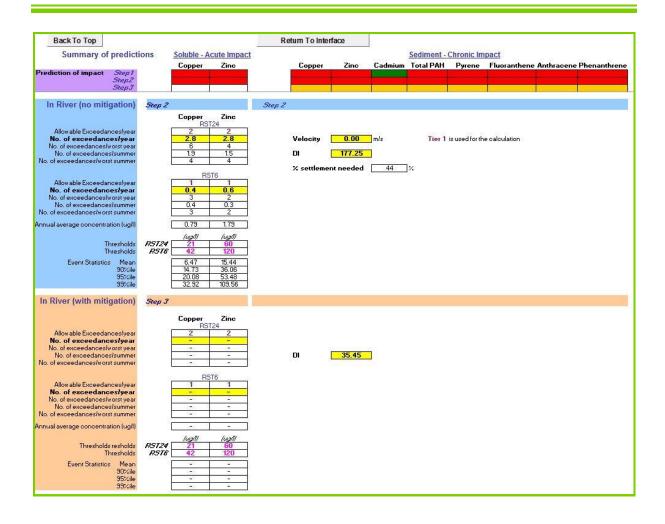


With Active Mitigation (vortex separator with assumed 80% removal of fine sediment)





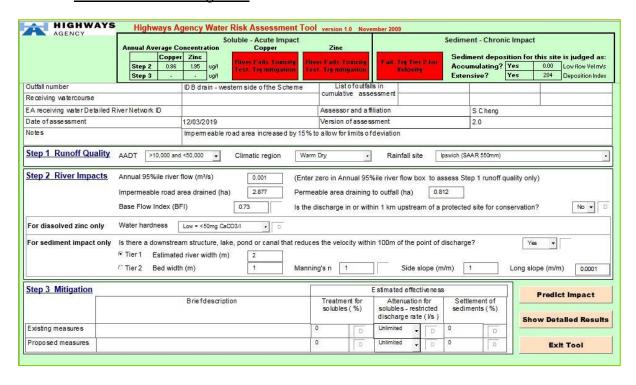




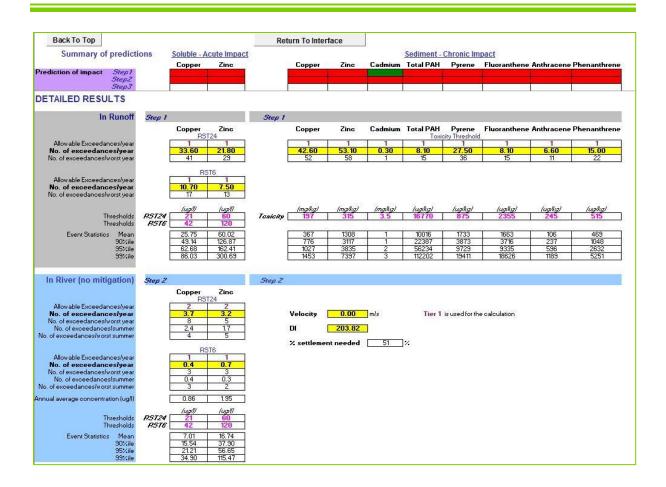


Scenario 1: Discharge to existing IDB watercourse (2.88ha impermeable area)

Without Active Mitigation



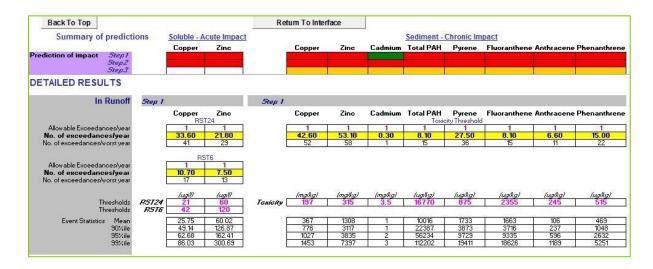




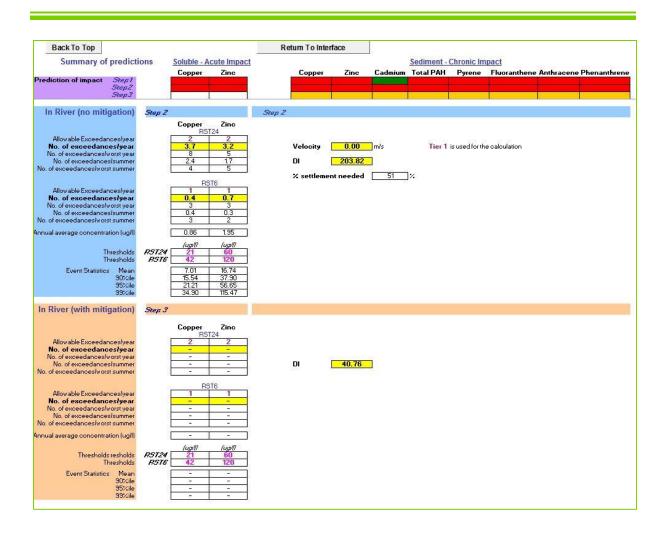


With Active Mitigation (vortex separator with assumed 80% removal of fine sediment)

HIGHWAYS	Highways A	gency Water	r Risk Assessment 1	ool vers	sion 1.0 Nove	mber 2009						
	Annual Average Co Copper Step 2 0.86 Step 3 -	oncentration	Copper River Fails Torreity Test. Try mitigation	River Fa	Zine ills Toricity mittigation	Stru	:. D/S cture.	Sedii Accu	ent - Chro ment depo imulating nsive?	osition fo	this site i	s judged as: .ow flow Vel m/s Deposition Index
Outfall number		IDB drain - we	stern side of the Scheme	cun	List of outfall							
Receiving watercourse				15								
EA receiving water Detailed Riv	erNetwork ID			100707	essor and a ff	100 C C C C C C C C C C C C C C C C C C			S C heng			
Date of assessment		12/03/2019		19.17101	sion of asses	7,000,000			2.0			
Notes		Impermeable	road area increased by 1	% to allo	w for limits of	deviation						
Step 1 Runoff Quality	AADT >10,000 and	<50,000 🔻	Climatic region	/arm Dry		Rainfal	l site	lpswich (S/	AAR 550mm)			
I	Annual 95%ile river mpermeable road a Base Flow Index (BR Water hardness	rea drained (ha	a) 2.877 Pe	rmeable a	in Annual 959 area draining arge in or with	to outfall (ha	a) 0.	812		68 18 spec		No ▼ □
		d river width (m	1 200	luces the	1/4	1,	ne point of de slope (i		e? 1		es •	0.0001
Step 3 Mitigation				7		E stimated e	ffective ne s	is.		76	Deadlet	Impact
		Briefdescription			atment for ubles (%)	solubles -				ttlement of iments (%)		
Existing measures				0	D	Unlimited	• D	0	D			
Proposed measures vortex s	eparator			0	D	Unlimited	- D	80	f		Exit	Tool









Scenario 2: Discharge to the River Yare (2.5ha impermeable area)

HIGHWAYS AGENCY	Highway													
AGENCY	Annual Averag	ge Concer	Soluble - Acute Impact Concentration Copper Zinc						Sediment - Chronic Impact					
		0.00 0.0		Pass		Pass		Alert, Pro Area		Accu	nent depo mulating? sive?		0.02 2	e is judged as: Low flow Vel m/s Deposition Index
utfall number	Ø.	Rive	r Yare - we	estern side ofthe	Scheme	List o	foutfalls				·			
le ceiving watercourse		- 3				6							- 3	
A receiving water Detailed R	tiver Network ID					Assessora	and a ffilia	ation			S C heng			
ate of assessment		0 1/0	3/2019			Version of	fassessn	ment			1.0			
o te s														
tep 1 Runoff Quality	AADT >10,00	00 and < 50,0	00 -	Climatic region	n Warm	Dry		Rainfall s	ite	lpswich (SA	AR 550mm)			
itep 2 River Impacts	Annual 95%ile	(3) (3		4.549	4 18.5			ile river flow	· person		p 1 runoff	quality or	nly)	
	Annual 95%ile i Impermeable ro Base Flow Inde	oad area d ex (BFI)		0.64	Perme	able area dr	raining to		0.8	112	(*) 2 - 201 - 102		154	Yes
or dissolved zinc only	Impermeable ro Base Flow Inde Water hardness Is there a down & Tier 1 Estir	oad area d ex (BFI) s Low =	<pre>crained (ha </pre> <pre><50mg CaC ucture, lak r width (m)</pre>	0.84 0.03/1 . (c., pond or canal	Perme	able area dr discharge in es the velocit	raining to	o outfall (ha) n 1 km upstre	0.8	protected discharge	site for co	nservatio	on?	D
for dissolved zinc only for sediment impact only	Impermeable ro Base Flow Inde Water hardness Is there a down & Tier 1 Estir	pad area d ex (BFI) s Low: nstream str	<pre>crained (ha </pre> <pre><50mg CaC ucture, lak r width (m)</pre>	0.84 0.03/1 . (c., pond or canal	Perme Is the o	able area dr discharge in es the velocit	or within	o outfall (ha) n 1 km upstre	0.sam of a	protected discharge	site for co	nservatio	on?	n) 0.0001
For dissolved zinc only For sediment impact only Step 3 Mitigation	Impermeable ro Base Flow Inde Water hardness Is there a down & Tier 1 Estir	oad area dex (BFI) s Low : nstream str mated rive width (m)	<pre>crained (ha </pre> <pre><50mg CaC ucture, lak r width (m)</pre>	2.502 0.84 0.84 0.84 0.84 0.84 0.84 0.84 0.84 0.84 1.00 1.00 1.00 1.00	Perme Is the o	able area dr discharge in es the velocit	or within	o outfall (ha) n 1 km upstre 100m of the	point of slope (rectivenesson for stricted	protected discharge n/m)	site for co	Long s	on?	n) 0.0001
For dissolved zinc only For sediment impact only	Impermeable ro Base Flow Inde Water hardness Is there a down & Tier 1 Estir	oad area dex (BFI) s Low : nstream str mated rive width (m)	rained (ha <50mg CaC ucture, lak r width (m)	2.502 0.84 0.84 0.84 0.84 0.84 0.84 0.84 0.84 0.84 1.00 1.00 1.00 1.00	Perme Is the deliberation of the deliberation	able area dr discharge in es the velocit ng's n 1	or within	o outfall (ha) 1 km upstre 100m of the Side Stimated effe Attenuati	point of slope (rectivenesson for stricted	protected discharge n/m)	d site for co	Long s	on?	n) 0.0001

Back To Top				Ret	urn To Inter	face],					
Summary of predict	ions	Soluble - A	cute Impact					Sediment -	Chronic Im	pact		
r		Copper	Zinc		Copper	Zinc	Cadmium	Total PAH	Pyrene	Fluoranthene	e Anthracene	Phenanthrene
ediction of impact Step 1 Step 2											-	
Step3										1		
ETAILED RESULTS												
In Runoff	Step 1			Step 1								
	100	Copper	Zinc		Copper	Zinc	Cadmium	Total PAH	Pyrene	Fluoranthene	e Anthracene	Phenanthrene
Allowable Exceedances/year		RS*			SERVICE OF SERVICE	1	4	Тохіс	city Threshold	1		1
No. of exceedances/year		33.60	21.80		42.60	53.10	0.30	8.10	27.50	8.10	6.60	15.00
No. of exceedances/worst year		41	29		52	58	1	15	36	15	11	22
		RS	ST6									
Allowable Exceedances/year		1 10 70	1									
No. of exceedances/year No. of exceedances/worst year		10.70 17	7.50 13									
		10.00	2 460		15 10000	15 1000	9 625	2 2 2	8 3 5	F1 142515		2 200
Thresholds	RST24	(capil)	(ugill)	Toxicity	(mg/kg/ 197	(mg/kg) 315	(mg/kg/ 3.5	(ug/kg) 16770	(ug/kg/ 875	(ug/kg/ 2355	(ug/kg/ 245	(ugikg) 515
Thresholds	RST6	42	120									
Event Statistics Mean		25.75	60.02	İ	367	1308	1 1	10016	1733	1663	106	469
90%ile 95%ile		49.14 62.68	126.87 162.41		776 1027	3117 3835	2	22387 56234	3873 9729	3716 9335	237 596	1048 2632
99%ile		86.03	300.69		1453	7397	3	112202	19411	18626	1189	5251
In River (no mitigation)	Step 2			Step 2								
		Copper	Zinc									
the second of the second		RS										
Allowable Exceedances/year No. of exceedances/year		0	0		0.1	0.02	m/s	T1 1	is used for th			
No. of exceedances/worst year		0	0		Velocity	0.02	mrs	Her I	is usea for th	e calculation		
No. of exceedances/summer		0	0		DI	2.71						
o. of exceedances/worst summer		0	0		% settlemer	at pooded	0	1%				
		RS	ST6		z. settlemer	it lieeded		17.				
Allowable Exceedances/year		0.5	0.5									
No. of exceedances/year No. of exceedances/worst year		0	0									
No. of exceedances/summer		ő	ŏ									
o, of exceedances/worst summer		0	0									
ual average concentration (ug/l)		0.00	0.00									
		(ugall)	(ugill)									
Thresholds	RST24	21	60									
Thresholds	RST6	42	120									
Event Statistics Mean 90%ile		0.00	0.01									



Scenario 2: Discharge to the River Yare (2.88ha impermeable area)

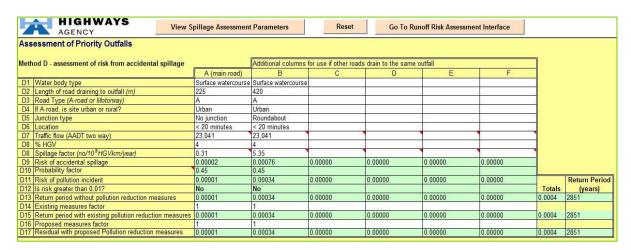
HIGHWAYS	Highways Agency Water Risk Assessment Tool version 1.0 November 2009										
AGENCY	Annual Average C Coppe Step 2 0.00 Step 3	oncentration	oluble - Acute Impac Copper Pass	Z	ine ass	Alert. Protec Area.	Sec Acc	liment depositi sumulating? Y ensive? N	ion for this site is judged as: es 0.02 Low flow Vel m/s		
Outfall number		River Yare - we	stern side of the Sche		List of outfal						
Receiving watercourse				Cum	iulative assi	essment					
EA receiving water Detailed R	iverNetwork ID			Asse	essor and a f	iliation		S C heng			
Date of assessment		12/03/2019		Vers	sion of asses	sment		2.0			
Notes		Impermeable r	oad area increased by	/15% to allow	w for limits of	deviation			3		
Step 1 Runoff Quality	AADT >10,000 and	i <50,000 →	Climatic region	Warm Dry		Rainfall site	lpswich (SAAR 550mm)			
For dissolved zinc only	Impermeable road a Base Flow Index (B Water hardness		0.73	Permeable a	rea draining	%ile river flow boo to outfall (ha) nin 1 km upstrean	0.812				
For sediment impact only		d river width (m	20 1000	reduces the Manning's n			int of dischar		No • 0		
Step 3 Mitigation						E stimated effecti	ve ne ss		Predict Impact		
		Brie fdescript	ion		atment for ubles (%)	solubles - restri	Attenuation for Settleme solubles - restricted sediments scharge rate (Vs.)		of		
Existing measures				0	D	Unlimited	D 0	D			
Proposed measures				0	D	Unlimited	D 0	D	Exit Tool		

Back To Top				Pot	urn To Inter	faco						
Summary of predictions		Soluble - Acute Impact Copper Zinc		Kei	88	Zinc] 	Sediment - Chronic Impact Total PAH				
Prediction of impact Step 1	179	Copper	Zine		Copper	Zinc	Cadmium	Total PAH	Pyrene	Fluoranthene	Anthracene	Phenanthrene
Step2 Step3	745							Ž.				
DETAILED RESULTS												
In Runoff	Step 1			Step 1								
		Copper RS1	Zinc		Copper	Zinc	Cadmium	Total PAH	Pyrene		Anthracene	Phenanthrene
Allowable Exceedances/year	70	16.	1		1	1	1.	1	1	1	1	1
No. of exceedances/year No. of exceedances/worst year		33.60 41	21.80 29		42.60 52	53.10 58	0.30	8.10 15	27.50 36	8.10 15	6.60 11	15.00 22
Allowable Exceedances/year No. of exceedances/year No. of exceedances/worst year	8	RS 1 10.70 17	T6 1 7.50 13	3		339			13090			
	2	(cognit)	(cogst)		(mg/kg/	(mg/kg/	(mg/kg/	(ug/kg/	(ug/kg/	(ug/kg/	(walky)	(cogillog)
Thresholds Thresholds	RST24 RST6	21 42	120	Toxicity	197	315	3.5	16770	875	2355	245	515
Event Statistics Mean	11010	25.75	60.02		367	1308	1 1	10016	1733	1 1663	106	T 469
90%ile		49.14	126.87		776	3117	1 1	22387	3873	3716	237	1048
95%ile 99%ile		62.68 86.03	162.41 300.69		1027 1453	3835 7397	2	56234 112202	9729 19411	9335 18626	596 1189	2632 5251
In River (no mitigation)	Step 2	Copper RS1	Zine 24	Step 2								
Allowable Exceedances/year No. of exceedances/year No. of exceedances/worst year No. of exceedances/summer No. of exceedances/worst summer		0 0 0	0 0		Velocity DI	0.02 3.29	mis	Tier 1	is used for th	e calculation		
Allowable Exceedances/year	38	RS 0.5	T6		% settleme	nt needed	0]%				
No. of exceedances/year No. of exceedances/worst year No. of exceedances/summer No. of exceedances/worst summer		0 0	0 0									
Annual average concentration (ug/l)		0.00	0.00									
Thresholds Thresholds	RST24 RST6	(ug/l) 21 42	(ugill) 60 120									
Event Statistics Mean 90%ile 95%ile 99%ile		0.00 0.01 0.01 0.04	0.01 0.02 0.03 0.11									



Annex B: Details of the Method D Assessment

Without Active Mitigation



With Active Mitigation (Spillage control penstocks)

